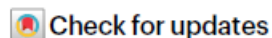


Spontaneous electrochemical uranium extraction from wastewater with net electrical energy production

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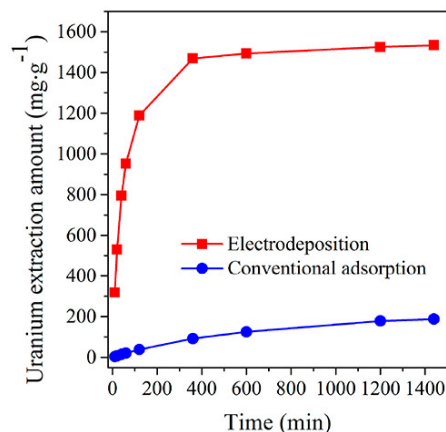
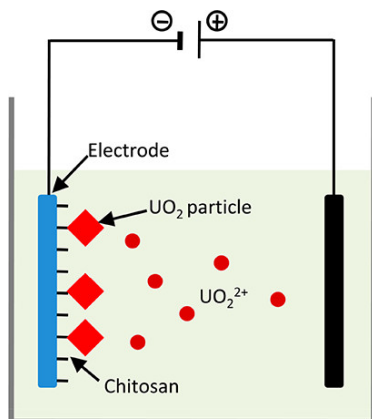
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Highly Efficient Recovery of Uranium from Seawater Using an Electrochemical Approach

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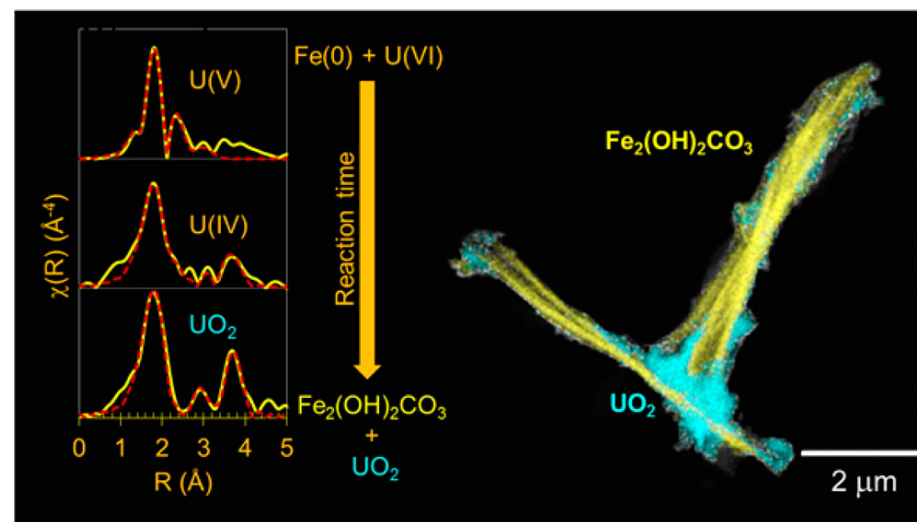


Reduced Uranium Phases Produced from Anaerobic Reaction with Nanoscale Zerovalent Iron

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Reductive Precipitation of Uranium(VI) by Zero-Valent Iron

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Introduction

- Here they reported a spontaneous electrochemical (SPEC) method driven by zero-valent iron (ZVI) oxidation for uranium extraction with simultaneous energy recovery.
- In the SPEC system, the U(VI) adsorption occurs on the surface of a porous carbonaceous cathode, while the oxidation of Fe^0 to Fe^{2+} takes place in the anodic chamber, providing electrons that flow through an external circuit to the cathode to drive the reduction of U(VI) to U(IV).
- The SPEC method has achieved a uranium extraction capacity of $2,438 \text{ mg g}^{-1}$ using simulated wastewater and 303 mg g^{-1} using real uranium mine wastewater without saturation, and the uranium extraction products are easily recoverable.
- The whole uranium extraction–recovery process requires no energy input, and net electrical energy production has been attained.

Why this paper?

- The system not only extracts uranium but also generates net electrical energy during the process. This dual function—resource recovery and energy production—adds significant value, making the method sustainable and energy-efficient.
- Interestingly, the reused electrode exhibited better uranium extraction performance than the fresh electrode.
- If the method is scalable, it could potentially be applied to various industrial sectors.

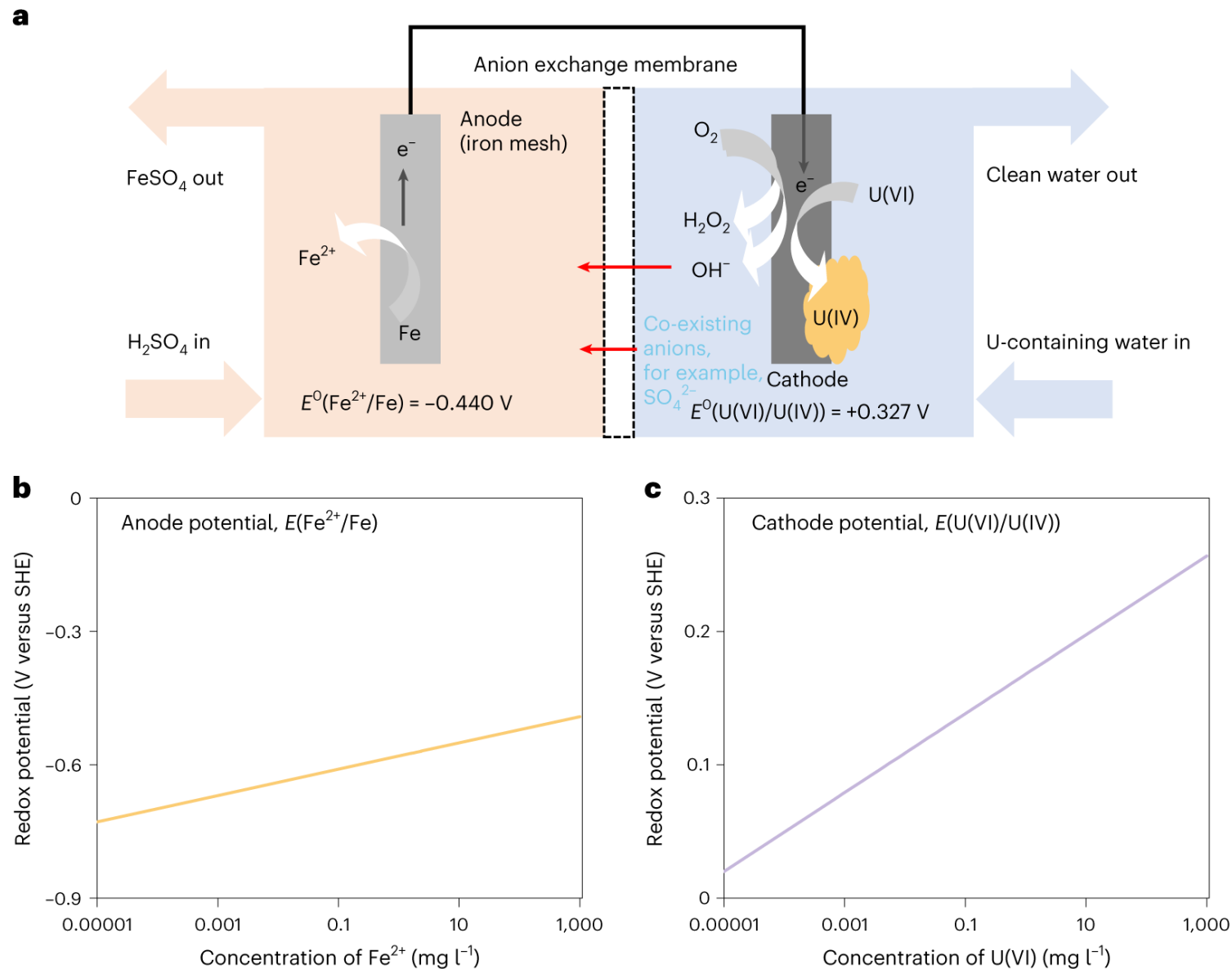


Fig. 1 Aschematic representation of the SPEC method and the calculated potentials. **a**, Aschematic representation of the SPEC uranium extraction method. **b**, The calculated anode potential as a function of Fe^{2+} concentration. **c**, The calculated cathode potential as a function of $U(VI)$ concentration.

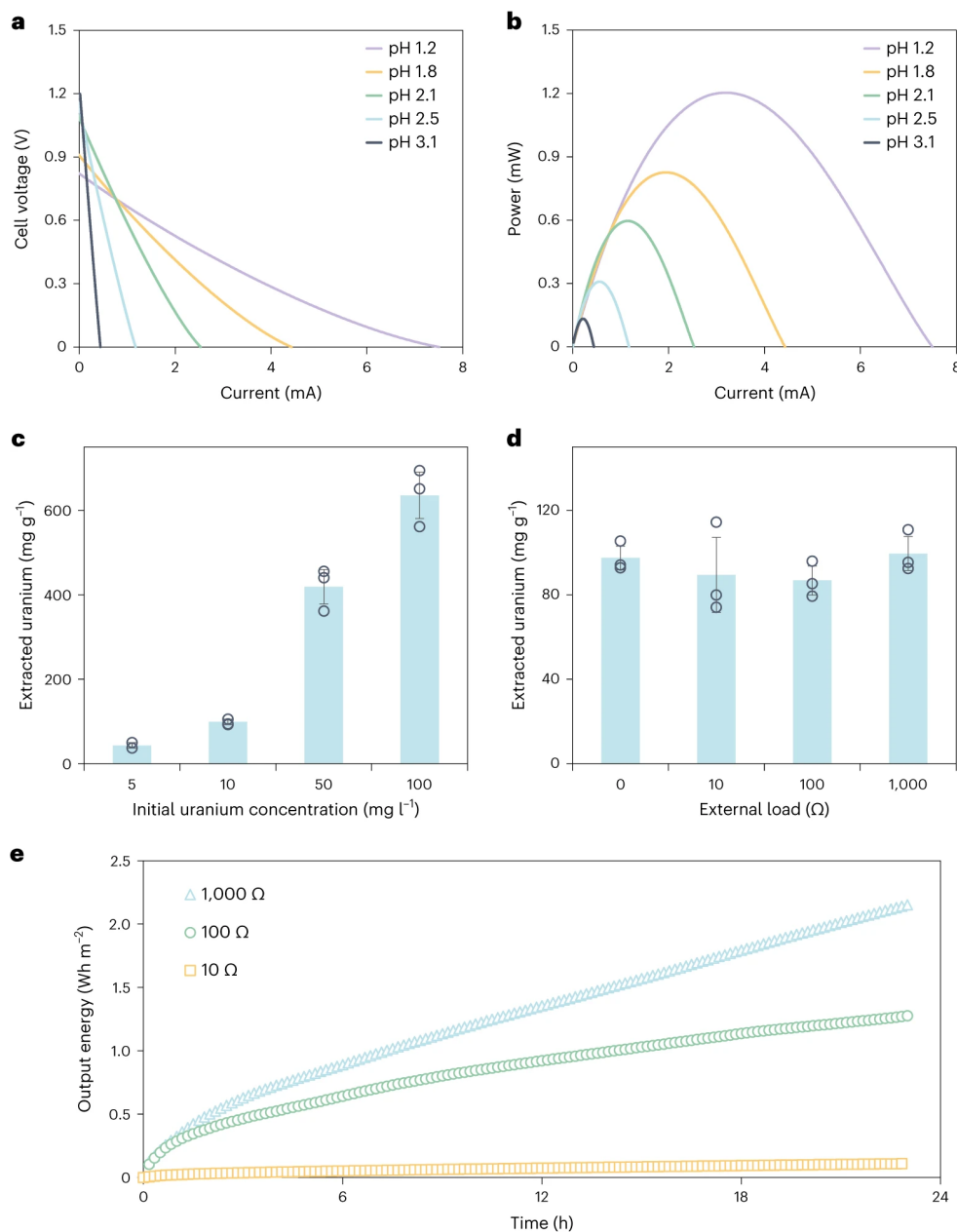


Fig. 2. Uranium extraction from water by the SPEC method with simultaneous energy recovery. **a**, Polarization curves of the SPEC system containing H₂SO₄ solution at varied pH as the anodic solution and simulated uranium-containing wastewater (10 mg l⁻¹) as the cathodic solution. **b**, The power of the SPEC system calculated according to the polarization curves. **c**, The total uranium extraction efficiency of the SPEC method after 23 h of operation using simulated uranium-containing wastewater with varied initial uranium concentration ([U]0). The data are presented as mean ± s.d. (n=3), while the overlaid dot plots are the corresponding data points. **d**, The total uranium extraction efficiency of the SPEC method after 23 h of operation using simulated uranium-containing wastewater ([U]0 = 10 mg l⁻¹) with varied external load. The data are presented as mean ± s.d. (n=3), while the overlaid dot plots are the corresponding data points. **e**, The accumulated output energy density as a function of the operating time during SPEC uranium extraction using simulated uranium-containing wastewater ([U]0 = 10 mg l⁻¹) with varied external load. The effective area of the CCF electrode was 2.5 cm².

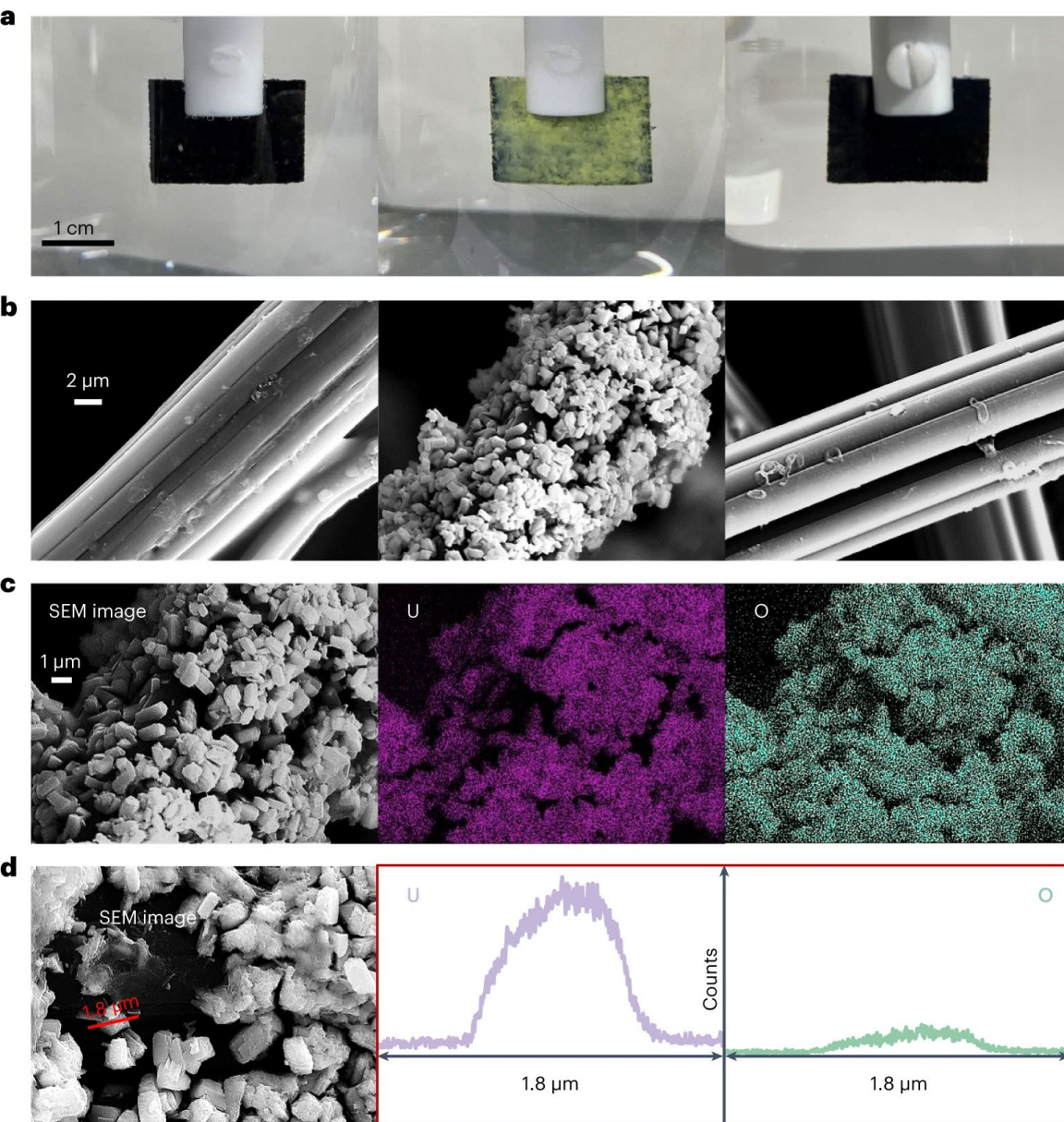


Fig. 3. Morphological characterizations of the extracted uranium. **a**, Photographs of the fresh CCF electrode (left), the CCF electrode after 23 h of uranium extraction via the SPEC method (centre) and the CCF electrode after 23 h of uranium extraction via the adsorption method (right). **b**, SEM images of the fresh CCF electrode (left) and the CCF electrode after 23 h of uranium extraction using the SPEC method (centre) and the adsorption method (right). **c**, EDS mapping showing the elemental composition of U (centre) and O (right) and distribution of the surface deposition layer (left) of the CCF electrode after SPEC uranium extraction. **d**, EDS line scans of U (centre) and O (right) along the red line across a microparticle (left) in the surface deposition layer shown in c. Conditions: simulated wastewater with $[U]_0 = 100 \text{ mg l}^{-1}$, unadjusted pH, without external load and effective area of CCF electrode of 2.5 cm^2 .

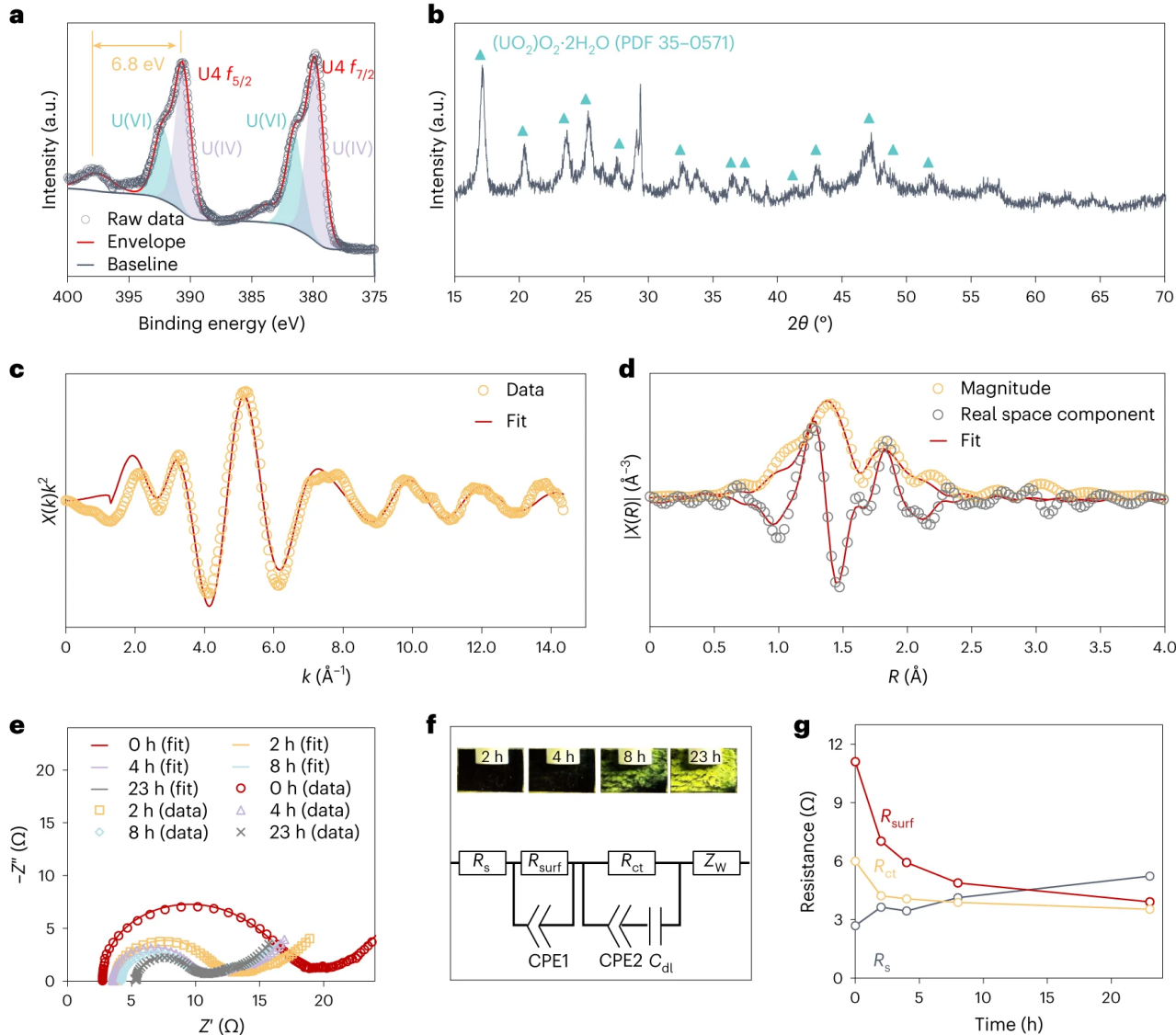


Fig. 4. Chemical properties of the extracted uranium. **a**, XPS U 4f spectrum. **b**, X-ray diffraction pattern. **c**, EXFAS k -space analysis. **d**, EXFAS R -space analysis of SPEC-extracted uranium species. **e**, Nyquist plots of the CCF electrode obtained by in situ EIS tests. **f**, The equivalent circuit used for electrochemical impedance spectroscopy (EIS) spectra fitting. C_{dl} , capacitance of the double layer; CPE, constant phase element. Inset: photographs of the CCF electrode during SPEC uranium extraction. **g**, The evolution of different resistance components derived from the Nyquist plots shown in **e**. Conditions: simulated wastewater with $[\text{U}]_0 = 100 \text{ mg l}^{-1}$, unadjusted pH, without external load and an effective area of the CCF electrode of 2.5 cm^2 .

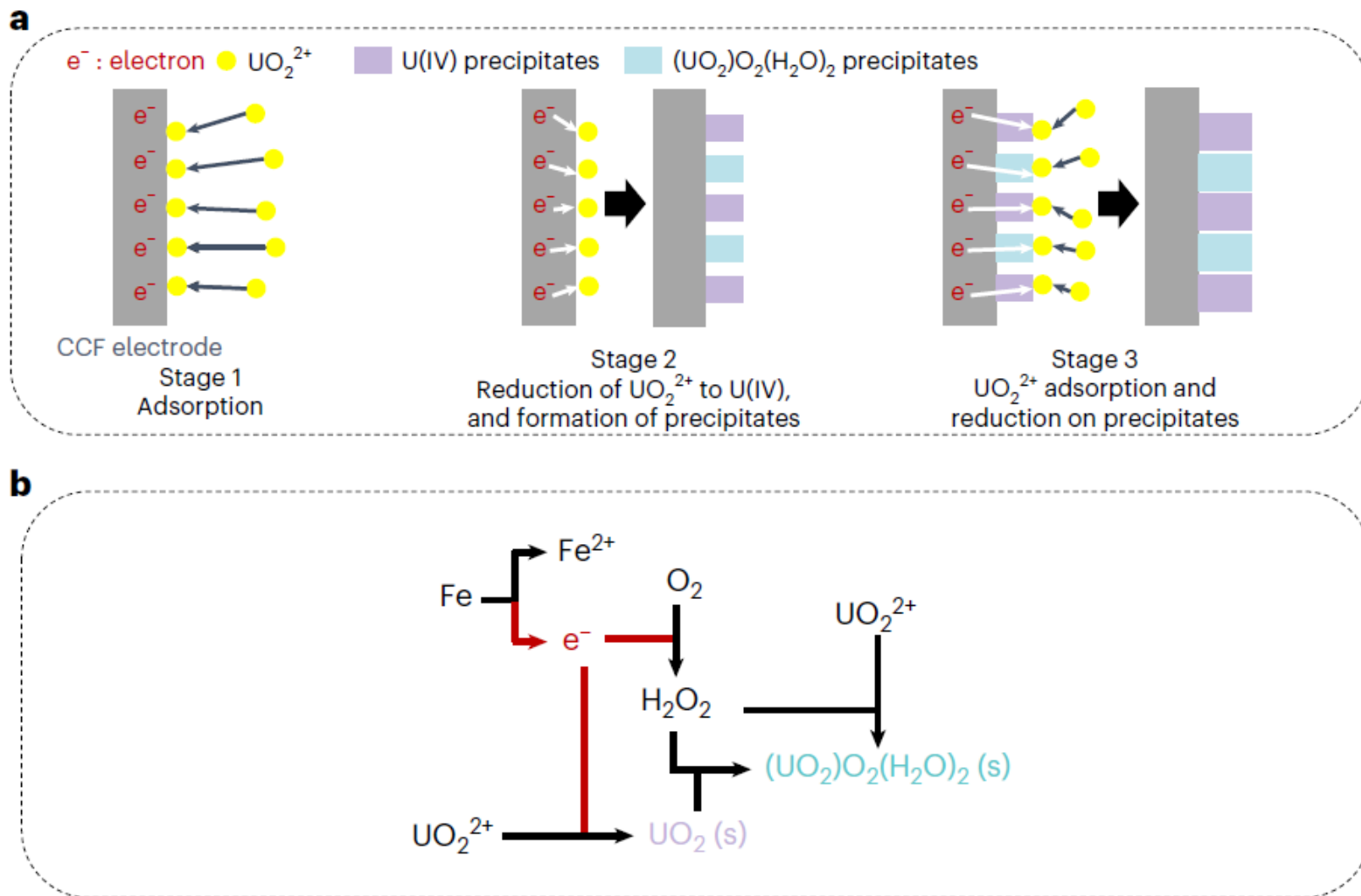


Fig. 5. Possible reactive pathways of the SPEC method. a,b, The proposed working mechanisms (a) and a schematic representation of the major reaction pathways (b) of the SPEC method.

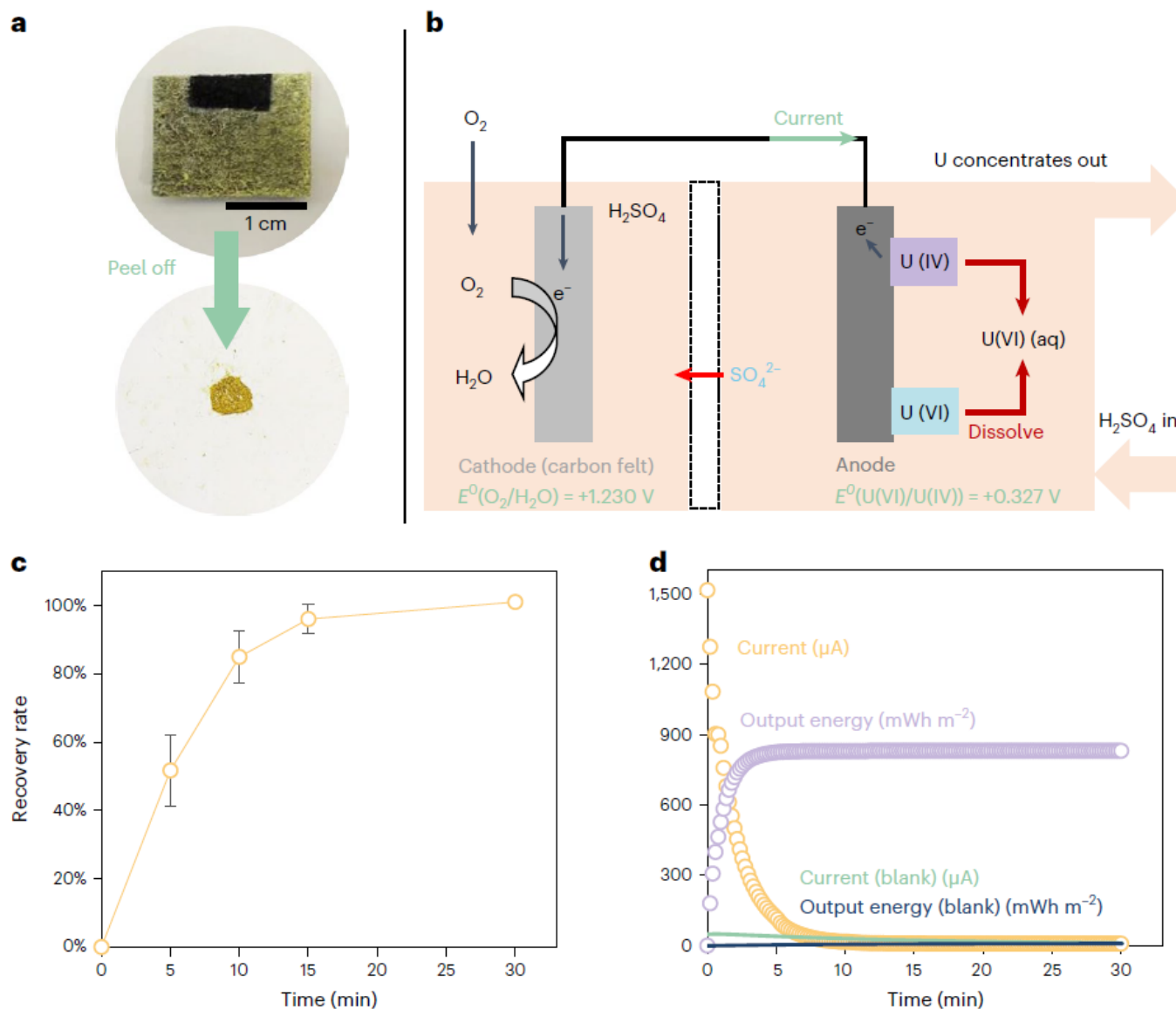


Fig. 6. Recovery of extracted uranium. **a**, Extracted uranium deposited on the surface of the electrode can be easily peeled off. **b**, A schematic representation of the U(IV)–DO cell concept for recovery of extracted uranium with simultaneous energy recovery. **c**, Uranium recovery using the U(IV)–DO cell. The data are presented as mean \pm s.d. ($n = 3$). **d**, The output current and the accumulated output energy density as functions of time during uranium recovery using the U(IV)–DO cell.

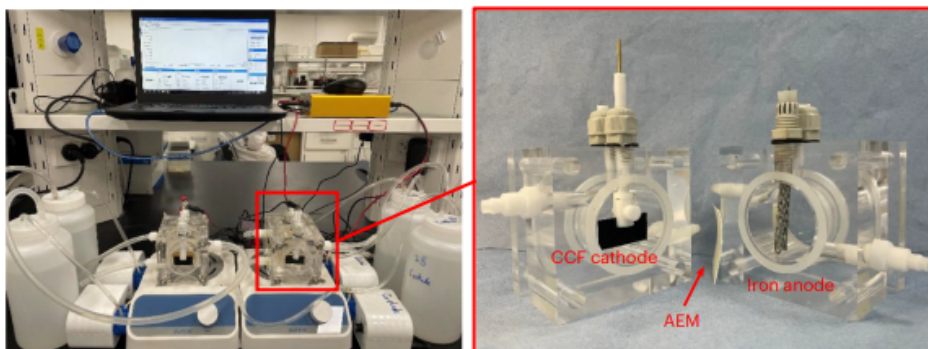
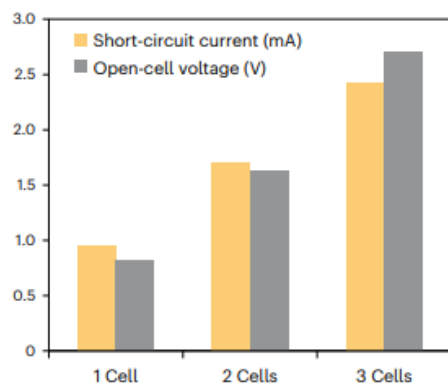
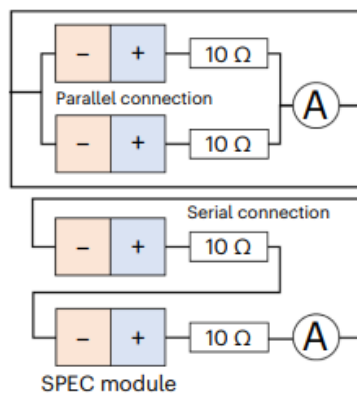
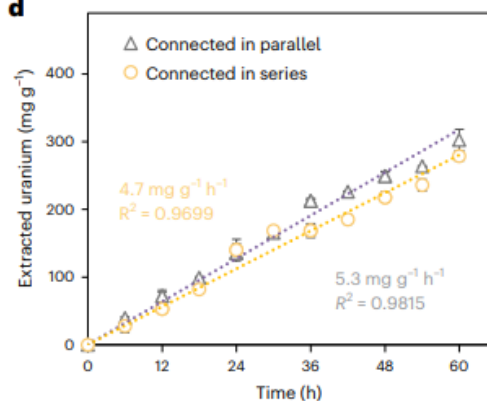
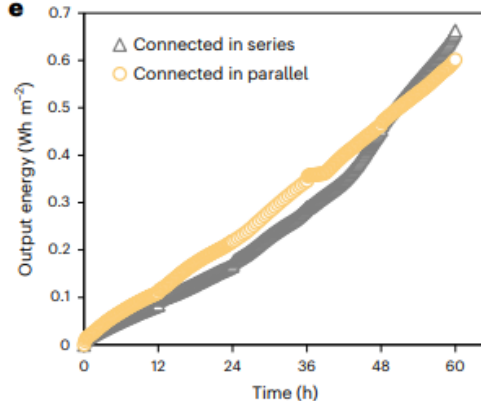
a**b****c****d****e**

Fig. 7. SPEC uranium extraction from real uranium mine wastewater. a, Photographs of the SPEC system (left) and cell (right) used for uranium extraction from real wastewater. AEM, anion exchange membrane. **b,** System OCV (connected in series) and SCC (connected in parallel) versus module number. **c,** The equivalent circuits of the two-module SPEC system connected in different modes. **d,** The long-term uranium extraction performance (data presented as mean \pm s.d. ($n=3$)). **e,** The electrical energy production performance of the SPEC system.

Conclusion

- They introduced a SPEC method powered by iron oxidation that can achieve efficient uranium extraction from real mine wastewater, with high stability.
- The formation of a uranium precipitates layer that provides reactive sites and conducts electron flows is the key to obtaining stable and efficient uranium extraction in electrochemical uranium extraction processes.
- Unlike conventional adsorption methods, the extraction products are ready to recover by peeling.
- In bench-scale SPEC uranium extraction experiments with real mine wastewater without process optimization, the operating cost for uranium extraction is calculated to be USD3.94–6.94 per kg of U.

Thank you